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A Generic Method for Modeling Accelerated Life Testing Data

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Key Words: accelerated life testing, Erlang-Coxian distribution, maximum likelihood estimation

SUMMARY & CONCLUSIONS

Accelerated life testing (ALT) is widely used to expedite failures of a product in a short time period for predicting the product's reliability under normal operating conditions. The resulting ALT data are often characterized by a probability distribution, such as Weibull, Lognormal, distribution, along with a life-stress relationship. However, if the selected failure time distribution is not adequate in describing the ALT data, the resulting reliability prediction would be misleading. This paper proposes a generic method that assists engineers in modeling ALT data. The method uses Erlang-Coxian (EC) distributions, which belong to a particular subset of phase-type (PH) distributions, to approximate the underlying failure time distributions arbitrarily closely. To estimate the parameters of such an EC-based ALT model, two statistical inference approaches are proposed. First, the moment-matching approach (method of moments) is developed to simultaneously match the moments of the ECbased ALT model to the ALT data collected at all test stress levels. In addition, the maximum likelihood estimation (MLE) approach is proposed to handle ALT data with type-I censoring. A numerical example is provided to illustrate the capability of the generic method in modeling ALT data.

1 INTRODUCTION

As technology advances, new products can be made quite reliable with high-performance materials and advanced system structures through efficient design tools. As a result, it is difficult, if not impossible, to observe failures of such a product in a short time period under its normal operating conditions for reliability estimation. To cope with today's fast paced technology innovation, accelerated life testing (ALT) has been widely used as a viable tool for estimating the long-term reliability of a new product. The basic idea of ALT is to expose some units of the product to harsher-than-normal operating conditions to expedite failures. Based on the resulting failure time data due to acceleration, a statistical model is developed and used to extrapolate the product's long-term reliability under the normal operating conditions.

Non-parametric methods are practical choices for predicting the reliability of a product without the need of knowing the underlying failure time distribution. The most popular ones include the Kaplan-Meier estimator and Breslow estimator [1]. However, it is difficult to extend such methods

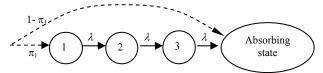
to develop ALT models which require the inclusion of various life-stress relationships (distribution parameters as functions of a set of stresses, or called covariates) in order to perform extrapolation with respect to both time and stresses. Because of this, the most popular methods in modeling ALT data are to develop a parametric model in the form of a probability distribution with a set of stress-dependent parameters. Such methods, if properly applied, are relatively efficient in terms of statistical inference, and the related inference procedures, such as maximum likelihood estimation (MLE) and least squares estimation (LSE), have been extensively studied and made available to practitioners [1]-[4].

Regarding the use of parametric ALT models in practice, practitioners often face the challenge of developing or selecting a parametric ALT model that provides an adequate fit to the collected data. Technically, several probability distributions may be considered as candidates, some of which may offer comparably good fits for the same data, e.g., see [5]-[7]. To determine the best model, the likelihood values or residual plots (e.g., Cox-Snell residuals) of these models can be considered. For relevant goodness-of-fit tests of ALT models, readers are referred to [8]. Indeed, several methods have been proposed to help practitioners overcome model selection problems to some extent. For example, Elsayed et al. [9] proposed the extended linear hazard regression model that is capable of modeling various ALT data and includes many ALT models as special cases. Moreover, Yu and Chang [10] proposed a Bayesian model-averaging approach to estimating life time quantiles in ALT by combining the lognormal and Weibull log-location-scale regression models. However, all these methods require extensive experience in modeling ALT and statistical inference. To assist engineers in implementing ALT, a generic method for modeling ALT data using a more versatile distribution would be desirable for a wide range of engineering applications.

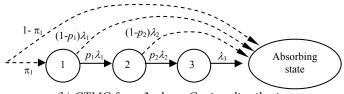
Phase-type (PH) distributions are a collection of stochastic models that represent the time to absorption of a continuous-time Markov chain (CTMC) defined on a finite-state space [11]. Figure 1 shows two examples, where the time until absorption to the respective absorbing state in each CTMC can be characterized by a PH distribution. Essentially, such a finite-state CTMC with the specific structure can be described by an infinitesimal generator matrix:

$$\mathbf{Q} = \begin{bmatrix} 0 & \mathbf{0} \\ \mathbf{S}^0 & \mathbf{S} \end{bmatrix},\tag{1}$$

where S is the subgenerator matrix consisting of the transition rates among transient states and the ones for transitions into the absorbing state(s), $S^0 = -S1$ and 1 = (1,1,...,1)'.



(a) CTMC for a 3-phase Erlang distribution



(b) CTMC for a 3-phase Coxian distribution Figure 1 - CTMCs Whose Absorption Times Define the Specific Phase-type Distributions

Let T be the time to absorption of a k-phase CTMC and $\mathbf{\pi} = (\pi_1, \pi_2, ..., \pi_k)$ be the initial distribution of the CTMC. The cumulative distribution function (cdf) of T is:

$$F(t) = 1 - \mathbf{\pi} \exp\{t\mathbf{S}\}\mathbf{1},\tag{2}$$

where $\exp\{t\mathbf{S}\}\$ is matrix exponential defined as:

$$\exp\{t\mathbf{S}\} = \sum_{k=0}^{\infty} \frac{1}{k!} (t\mathbf{S})^k. \tag{3}$$

The probability density function (pdf) of T is given by:

$$f(t) = \mathbf{\pi} \exp\{t\mathbf{S}\} \mathbf{S}^0, \tag{4}$$

and the hazard function can be expressed as:

$$h(t) = \pi \exp\{tS\}S^{0}/(\pi \exp\{tS\}1), t \ge 0.$$
 (5)

In addition, the lth moment of the distribution is given by:

$$E[T^{l}] = (-1)^{l} l! \, \pi S^{-l} \mathbf{1}. \tag{6}$$

For examples, the CTMC in Figure 1(a) results in a three-phase Erlang distribution $E(3,\lambda)$ with:

$$\mathbf{\pi} = (1,0,0) \text{ and } \mathbf{S} = \begin{bmatrix} -\lambda & \lambda & 0 \\ 0 & -\lambda & \lambda \\ 0 & 0 & -\lambda \end{bmatrix},$$

and the one in Figure 1(b) gives a three-phase Coxian distribution $C(\lambda_1, \lambda_2, \lambda_3, p_1, p_2)$ with:

$$\mathbf{\pi} = (1,0,0) \text{ and } \mathbf{S} = \begin{bmatrix} -\lambda_1 & p_1 \lambda_1 & 0 \\ 0 & -\lambda_2 & p_2 \lambda_2 \\ 0 & 0 & -\lambda_3 \end{bmatrix},$$

where $0 < p_i \le 1$, i = 1,2.

One of the most attractive properties of PH distributions is that the set of PH distributions is dense in the set of nonnegative distributions [12]. In other words, in theory, any nonnegative distribution can be approximated arbitrarily closely by a PH distribution. The only limitation of PH distributions is that they are light-tailed, thus may not be used as effective models for heavy-tailed distributions. Among different subsets of PH distributions, Erlang distributions and Coxian distributions are probably the two most popular ones. They have been extensively studied as part of queueing theory and widely used in healthcare such as survival data analysis and modeling the length of stay of patients in hospital [13,14].

Motivated by the versatility of PH distributions that naturally meets the broad requirements for parametric

modeling of failure time data, we propose a generic method using a specific and yet flexible subset of PH distributions, called Erlang-Coxian (EC) distributions [15], to model ALT data. Both moment-matching and MLE approaches are studied for statistical inference. This generic method contributes to the body of ALT literature in two ways. First, the use of EC distributions relaxes strong assumptions about the underlying failure time distributions in developing parametric ALT models. Moreover, for a specific set of ALT data, it is quite straightforward to adaptively adjust the number of phases of the associated CTMC to achieve the best fit based on statistical inference results.

2 DEVELOPMENT OF EC-BASED ALT MODEL

2.1 Basics of EC Distributions

Before we proceed with the proposed EC-based ALT model, we first introduce the following definitions [15].

Definition 1. Let $E[X^l]$ be the l^{th} moment of random variable X with distribution G. The normalized l^{th} moment m_l^G of X for l=2,3 is defined as: $m_2^G = \frac{E[X^2]}{(E[X])^2}$ and $m_3^G = \frac{E[X^3]}{E[X]E[X^2]}$.

Definition 2. A distribution G is well represented by a distribution F if F and G agree on their first three moments. PH_3 refers to the set of distributions that are well represented by a PH distribution.

It is known that a distribution G is in PH_3 if and only if its normalized moments satisfy $m_3^G > m_2^G > 1$ [16]. Since any nonnegative distribution G satisfies $m_3^G \ge m_2^G \ge 1$ [17], almost all the nonnegative distributions are in PH_3 . Osogami and Harchol-Balter [15] introduced the EC distributions, which are quite efficient for approximating PH_3 distributions. Figure 2 shows the CTMC for a k-phase EC distribution $(k \ge 3)$, which consists of an Erlang with k-2 phases: $E(k - 2, \lambda_1)$ and a two-phase Coxian: $C(\lambda_2, \lambda_3, p_c)$, for which:

$$\mathbf{S} = \begin{bmatrix} -\lambda_{1} & \lambda_{1} & 0 & \cdots & & & \\ 0 & -\lambda_{1} & \lambda_{1} & 0 & & \mathbf{0} \\ \vdots & 0 & -\lambda_{1} & \ddots & \ddots & & \vdots \\ & 0 & \ddots & \lambda_{1} & 0 & & \\ \vdots & & \ddots & -\lambda_{1} & \lambda_{1} & 0 & \\ \mathbf{0} & & 0 & -\lambda_{2} & p_{c}\lambda_{2} \\ & \cdots & \cdots & 0 & -\lambda_{3} \end{bmatrix}, (7)$$

and $\pi = (\underbrace{1,0,...,0}_{k \text{ terms}})$.

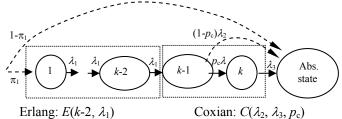


Figure 2 - CTMC for a k-phase EC Distribution

The idea of creating an EC distribution is that a two-phase Coxian distribution can well represent any distribution that has high second and third moments while an Erlang distribution has only two free parameters and has the least normalized second moment among all the PH distributions with a fixed number of phases. Therefore, such a k-phase EC distribution can represent probability distributions with all ranges of variability using only a small number of phases. This is important in developing a PH-based ALT model, which needs additional parameters for the life-stress relationship.

2.2 Formulation of EC-based ALT Model

Accelerated failure time (AFT) models are probably the most widely used parametric ALT models. Unlike a proportional hazards model, an AFT model assumes that the effect of a covariate is to multiply the failure time, instead of the hazard function, by some constant [9]. Mathematically, an AFT model for the cdf F(t; Z) of failure time under a constant stress Z can be expressed as [8]:

$$F(t;Z) = F_0(r(Z;\theta)t), \tag{8}$$

where $F_0(\cdot)$ is the baseline cdf and $r(Z; \underline{\theta})$ is a deterministic function of Z. Equivalently, this model can be expressed in terms of the corresponding hazard rate:

$$h(t;Z) = h_0(r(Z;\theta)t)r(Z;\theta), \tag{9}$$

where $h_0(\cdot)$ is the corresponding baseline hazard rate. An important aspect of implementing an AFT model is to assume the underlying failure time distribution, i.e., $F_0(\cdot)$.

Following Eqs. (2) and (8), the EC-based AFT model for a product's failure time under stress level *Z* is given by:

$$F(t;Z) = F_0(r(Z;\underline{\theta})t) = 1 - \pi \exp\{r(Z;\underline{\theta})tS\}\mathbf{1},$$
 (10 where π and S are given in Eq. (9). The corresponding pdf is:

$$f(t;Z) = r(Z;\underline{\theta})\pi \exp\{r(Z;\underline{\theta})tS\} S^{0}, \tag{11}$$

and the hazard function is:

$$h(t; Z) = r(Z; \underline{\theta}) \pi \exp \{r(Z; \underline{\theta}) t S\} S^{0} / (\pi \exp \{r(Z; \underline{\theta}) t S\} 1). \quad (12)$$

The corresponding l^{th} moments can be expressed as:

$$E[T_Z^l] = (-1)^l (r(Z; \underline{\theta}))^{-l} l! \, \mathbf{\pi} \mathbf{S}^{-l} \mathbf{1}, \tag{13}$$

3 STATISTICAL INFERENCE

This section addresses two statistical methods for estimating the parameters of an EC-based ALT model.

3.1 Moment-Matching (Method of Moments)

For complete ALT data, the l^{th} sample moment of failure

times
$$t_{ij}$$
 at stress level Z_i can be obtained as: $\frac{1}{n_i} \sum_{j=1}^{n_i} t_{ij}^l$. The

mathematical formulation for determining the matching EC-based AFT model with the least number of phases (i.e., k) can be expressed as:

Subject to
$$\frac{\left|\frac{(-1)^{1}(r(Z_{i};\underline{\theta}))^{-1}1!\boldsymbol{S}^{-1}\mathbf{1} - \frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}}{\frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}}\right| \leq \varepsilon_{i,1},$$

$$\frac{\left|\frac{(-1)^{2}(r(Z_{i};\underline{\theta}))^{-2}2!\boldsymbol{S}^{-2}\mathbf{1} - \frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}^{2}}{\frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}^{2}}\right| \leq \varepsilon_{i,2},$$

$$\frac{\left|\frac{(-1)^{3}(r(Z_{i};\underline{\theta}))^{-3}3!\boldsymbol{S}^{-3}\mathbf{1} - \frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}^{3}}{\frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}^{3}}\right| \leq \varepsilon_{i,3}, \quad i = 1,...,M,$$

$$\frac{1}{n_{i}}\sum_{j=1}^{n_{i}}t_{ij}^{3}$$

where $\varepsilon_{i,l}$ are the pre-specified levels of tolerance for each stress level Z_i . Note that the size of matrix S increases as the value of k increases, which only increases the number phases in Erlang $E(k-2, \lambda_1)$. The limitation of this approach is that extensive computational effort must be taken to find the solution that satisfies those nonlinear constraints, which may not be an easy task.

3.2 MLE method

We now consider a more complex case of constant-stress ALT experiment with Type-I censoring. Again, let t_{ij} be the recorded failure/censoring time of unit j tested under stress level Z_i , i=1,2,...,M, and n_i be the total number of units tested under Z_i .

The MLE method is widely used, which can handle different types of censored data quite efficiently. For ALT data with type-I censoring, the log-likelihood function *lnL* can be expressed as:

$$lnL(k, \lambda_{1}, \lambda_{2}, \lambda_{3}, p_{c}, \underline{\theta}) = \sum_{i=1}^{M} \sum_{j=1}^{n_{i}} [\delta_{ij} \log(f(t_{ij}; Z_{i})) + (1 - \delta_{ij}) \log(1 - F(t_{ij}; Z_{i}))]$$

$$= \sum_{i=1}^{m} \sum_{j=1}^{n_{i}} \delta_{ij} \log(r(Z_{i}; \underline{\theta}) \mathbf{\pi} \exp\{r(Z_{i}; \underline{\theta}) t_{ij} \mathbf{S}\} \mathbf{S}^{\mathbf{0}}) + (1 - \delta_{ij}) \log(\mathbf{\pi} \exp\{r(Z_{i}; \underline{\theta}) t_{ij} \mathbf{S}\} \mathbf{1}). \tag{15}$$

where $\delta_{ij} = \{1, \text{ if } t_{ij} \text{ is a failure time; 0, otherwise}\}$. The MLEs of the model parameters can be obtained by maximizing the log-likelihood function. In practice, different optimization algorithms, such as Quasi-Newton and Nelder-Mead algorithms, can be used.

3.3 Determination of The Number of Phases (Value of k)

A practical issue in developing an EC-based ALT model based on likelihood is to determine the number of phases, i.e., the value of k. For such model selection problems, the Akaike information criterion (AIC) can be utilized, which is expressed as:

$$AIC = 2q - 2lnL(k, \lambda_1, \lambda_2, \lambda_3, p_c, \theta), \tag{16}$$

where q is the number of parameters, which is the same for EC-based ALT models when the number of parameters in θ is

fixed. As a result, it is straightforward to compare the likelihood values when comparing candidate EC-based ALT models with different numbers of phases in order to determine the best one.

Note that the likelihood-ratio test has been widely used to test against nested models, which may not be appropriate for determining the number of phases in the EC-based ALT model.

4 NUMERICAL EXAMPLE

The ALT data reported by Liao and Elsayed [18] is used to illustrate the use of the proposed method in practice.

4.1 Experiment

The purpose of this ALT experiment is to estimate the reliability of a type of miniature lamps under the use condition: 2 volts. The highest operating voltage of the lamp is 5 volts. It is well known that the coil temperature of an incandescent lamp during operation is mainly due to the electric current. Three constant voltage levels were utilized in the experiment: 5 volts, 3.5 volts, and 2 volts. Table 1 gives the observed failure times and censoring times under the three stress levels.

Stress level	Failure times					
Suess level	("+": the unit is censored)					
5 volts	20.5	22.3	23.2	24.7	26	
	34.1	39.6	41.8	43.6	44.9	
	47.7	61.6	62.1	65.5	70.8	
	87.8	118.3	120.1	145.4	157.4	
	180.9	187.7	204	206.7	213.9	
	215.2	218.7	254.1	262.6	293	
	304	313.7	314.1	317.9	337.7	
	430.2					
3.5 volts	37.8	43.6	51.1	58.6	65.5	
	65.9	75.6	82.5	88.1	89	
	106.6	113.1	121.1	121.5	128.3	
	151.8	171.7	181	202.7	211.7	
	230.7	249.9	275.6	285	296.2	
	358.5	379.8	434.5	493.1	506.4	
	561.1	570	577.7	876.3	922	
	890+	890+	890+	941+	941+	
2 volts	223.1	254	316.7	560.2	679	
	737	894.4	930.5+	930.5+		
	930.5+	930.5+	930.5+	930.5+		
	930.5+	930.5+	930.5+	930.5+		
	930.5+	930.5+	930.5+	930.5+		
	930.5+	930.5+	930.5+			

Table 1 - ALT Data of Miniature Lamps

Figure 3 shows the empirical cdf (Kaplan-Meier) of the lamp under each different voltage level. To avoid making an assumption on the underlying distribution, such as Weibull and Lognormal, we use the proposed EC-based ALT model to predict the reliability of this type of miniature lamps.

4.2 EC-based ALT Model and Estimation Results

To facilitate data analysis, we standardize the stress levels by defining $Z_i = [V_i - V_0]/[V_H - V_0]$, where $V_0 = 2$ volts and $V_H = 5$ volts. As a result, we have: $Z_1 = 1$, $Z_2 = 0.5$, and $Z_3 = 0$. The life-stress relationship is assumed to be characterized by:

$$r(Z_i; \underline{\theta}) = \exp(\alpha_0 Z_i^{\alpha_1}). \tag{17}$$

Because the data set contains censoring times, we use the MLE method introduced in section 3.2 for statistical inference. Table 2 shows the MLEs of model parameters for different EC-based ALT models with different numbers of phases. By comparing the log-likelihood values, the EC-based ALT model with k=5 phases is selected after balancing the prediction accuracy and the complexity of the models.

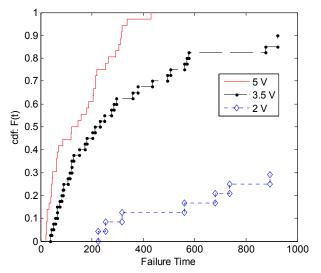


Figure 3 - Empirical cdf's of the Failure Times under Different Voltage Levels

Values of k	MLEs of	Log-likelihood	
values of K	parameters	lnL	
3: $E(1, \lambda_1)$ & $C(\lambda_2, \lambda_3, p_c)$	$\alpha_0 = 2.9091;$		
	$\alpha_1 = 0.5762;$	-518.5038	
	$\lambda_1 = 0.0026;$		
	$\lambda_2 = 0.0026;$		
	$\lambda_3 = 0.0003;$		
	$p_c = 0.6730;$		
4: $E(2, \lambda_1)$ & $C(\lambda_2, \lambda_3, p_c)$	$\alpha_0 = 2.8807;$		
	$\alpha_1 = 0.5730;$		
	$\lambda_1 = 0.0045;$	516 4050	
	$\lambda_2 = 0.0045;$	-516.4058	
	$\lambda_3 = 0.0003;$		
	$p_c = 0.6980;$		
5: $E(3, \lambda_1)$ & $C(\lambda_2, \lambda_3, p_c)$	$\alpha_0 = 2.8182;$		
	$\alpha_1 = 0.5693$;		
	$\lambda_1 = 0.0068;$	515 4042	
	$\lambda_2 = 0.0068;$	-515.4942	
	$\lambda_3^2 = 0.0004;$		
	$p_c = 0.7269;$		
6: $E(4, \lambda_1)$ & $C(\lambda_2, \lambda_3, p_c)$	$\alpha_0 = 2.7463;$		
	$\alpha_1 = 0.5747;$	-515.0856	
	$\lambda_1 = 0.0097;$		

$\lambda_2 = 0.0097;$	
$\lambda_3 = 0.0004;$	
$p_c = 0.7545;$	

Table 2 - MLEs of Parameters for Different EC-based ALT Models with Different Numbers of Phases (k)

Figure 4 illustrates the statistical fittings of the resulting EC-based ALT model for the three test stress levels. Compared to the corresponding empirical cdf's, this model exhibits satisfactory prediction capability. Figure 5 shows the predicted reliability function, pdf and hazard rate of the lamp under the normal operating condition. The mean-time-to-failure can be easily obtained as 2405.5 hours.

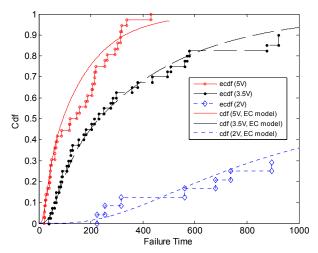


Figure 4 - Statistical Fittings of the Resulting Model

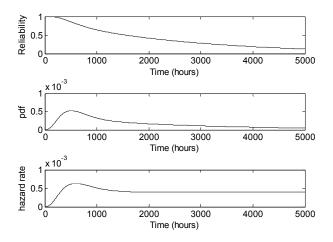


Figure 5 - Reliability Prediction using the Resulting Model (reliability function, pdf, hazard rate under 2V)

5 CONCLUSIONS

Although the applications of PH distributions have been studied in other areas, such as queueing systems and healthcare, they have not been used in modeling ALT. This paper introduces a generic method for modeling ALT data using EC distributions, which belong to an important subset of PH distributions. Without assuming other particular probability distributions for failure times, such as extreme

value distributions (Gumbel, Weibull, and Fréchet distributions), lognormal distribution, and mixture of distributions, this method leads to an EC-based ALT model which can well represents the underlying failure time distribution that may be unknown and/or difficult to verify. Both moment-matching approach and MLE approach are developed for parameter estimation. The technical contribution of this paper is to demonstrate, for the first time, the potential of using PH distributions in developing ALT models. The numerical example demonstrates that the method indeed provides practitioners with a powerful tool for modeling ALT data.

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REFERENCES

- Meeker, W.Q. and Escobar, L.A., Statistical Methods for Reliability Data, John Wiley & Sons, New York, New York, 1998.
- Nelson, W.B., Accelerated Testing Statistical Models, Test Plans, and Data Analysis, John Wiley & Sons, Hoboken, New Jersey, 1990.
- 3. Elsayed, E.A., *Reliability Engineering*, Addison Wesley Longman, New York, New York, 1996.
- 4. Yang, G., *Life Cycle Reliability Engineering*, John Wiley & Sons, Inc., Hoboken, NJ, USA, 2007.
- 5. Lawless, J.F. and Singhal, K., "Analysis of data from lifetest experiments under an exponential model", *Naval Research Logistics Quarterly*, vol. 27, no. 2, 1980, p 323 334.
- Doksum, K.A. and Hóyland, A., "Models for variablestress accelerated life testing experiments based on Wiener processes and the inverse Gaussian distribution", *Technometrics*, vol. 34, no. 1, 1992, p 74 – 82.
- Escobar, L.A. and Meeker, W.Q., "A review of accelerated test models", *Statistical Science*, vol. 21, no.4, 2006, p 552 – 577.
- 8. Bagdonavičius, V. and Nikulin, M., Accelerated Life Models Modeling and Statistical Analysis, Chapman & Hall/CRC, New York, New York, 2002.
- Elsayed, E.A., Liao, H.T., and Wang, X.D., "An extended linear hazard regression model with application to timedependent-dielectric-breakdown of thermal oxides", *IIE Transactions*, vol. 38, no. 4, 2006, p 329-340.
- Yu, I.T. and Chang, C.L., "Applying Bayesian model averaging for quantile estimation in accelerated life tests", *IEEE Transactions on Reliability*, vol. 61, no. 1, 2012, p 74-83.
- 11. Altiok, T., "On the phase-type approximations of general distributions", *IIE Transactions*, vol. 17, 1985, p 110–116.
- 12. Nelson, R., *Probability, Stochastic Processes, and Queueing Theory The Mathematics of Computer Performance Modeling*, Springer-Verlag, New York, New

- York, 1995.
- 13. Marshall, A.H. and Zenga, M., "Simulating Coxian phase-type distributions for patient survival", *International Transactions in Operational Research*, vol. 16, no. 2, 2009, p 213-226.
- Marshall, A.H. and McClean, S.I., "Using Coxian phasetype distributions to identify patient characteristics for duration of stay in hospital", *Health Care Management Science*, vol. 7, no.4, 2004, p 285-289.
- Osogami, T. and Harchol-Balter, M., "Closed form solutions for mapping general distributions to quasiminimal PH distributions", *Performance Evaluation*, vol. 63, 2006, p 524–552.
- 16. Johnson, M.A. and Taaffe, M.R., "Matching moments to phase distributions: Mixtures of Erlang distributions of common order", *Communications in Statistics Stochastic Models*, vol. 5, 1989, p 711 743.
- 17. Karlin, S. and Studden, W., *Tchebycheff Systems: With Applications in Analysis and Statistics*. John Wiley and Sons, 1966.
- 18. Liao, H.T. and Elsayed, E.A., "Equivalent accelerated life testing plans for log- location-scale distributions", *Naval Research Logistics*, vol. 57, no. 5, 2010, p 472-488.

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Dr. Huairui (Harry) Guo is the Director of the Theoretical Development Department at ReliaSoft Corporation. He received his Ph.D. in Systems & Industrial Engineering and M.S. in Reliability & Quality engineering; both from the University of Arizona. His research and publications cover reliability areas, such as life data analysis, repairable system modeling and reliability test planning, and quality areas, such as process monitoring, analysis of variance and design of experiments. In addition to research and product development, he is also part of the training and consulting arm and has been involved in various projects from automobile, medical device, oil and gas, and aerospace industry. He is a certified reliability professional (C.R.P), ASQ certified CQE. He is a member of IIE, SRE and ASQ.